

# Vector Formulas

$$\begin{aligned}
 \mathbf{a} \cdot (\mathbf{b} \times \mathbf{c}) &= \mathbf{b} \cdot (\mathbf{c} \times \mathbf{a}) = \mathbf{c} \cdot (\mathbf{a} \times \mathbf{b}) \\
 \mathbf{a} \times (\mathbf{b} \times \mathbf{c}) &= (\mathbf{a} \cdot \mathbf{c})\mathbf{b} - (\mathbf{a} \cdot \mathbf{b})\mathbf{c} \\
 (\mathbf{a} \times \mathbf{b}) \cdot (\mathbf{c} \times \mathbf{d}) &= (\mathbf{a} \cdot \mathbf{c})(\mathbf{b} \cdot \mathbf{d}) - (\mathbf{a} \cdot \mathbf{d})(\mathbf{b} \cdot \mathbf{c}) \\
 \nabla \times \nabla\psi &= 0 \\
 \nabla \cdot (\nabla \times \mathbf{a}) &= 0 \\
 \nabla \times (\nabla \times \mathbf{a}) &= \nabla(\nabla \cdot \mathbf{a}) - \nabla^2\mathbf{a} \\
 \nabla \cdot (\psi\mathbf{a}) &= \mathbf{a} \cdot \nabla\psi + \psi\nabla \cdot \mathbf{a} \\
 \nabla \times (\psi\mathbf{a}) &= \nabla\psi \times \mathbf{a} + \psi\nabla \times \mathbf{a} \\
 \nabla(\mathbf{a} \cdot \mathbf{b}) &= (\mathbf{a} \cdot \nabla)\mathbf{b} + (\mathbf{b} \cdot \nabla)\mathbf{a} + \mathbf{a} \times (\nabla \times \mathbf{b}) + \mathbf{b} \times (\nabla \times \mathbf{a}) \\
 \nabla \cdot (\mathbf{a} \times \mathbf{b}) &= \mathbf{b} \cdot (\nabla \times \mathbf{a}) - \mathbf{a} \cdot (\nabla \times \mathbf{b}) \\
 \nabla \times (\mathbf{a} \times \mathbf{b}) &= \mathbf{a}(\nabla \cdot \mathbf{b}) - \mathbf{b}(\nabla \cdot \mathbf{a}) + (\mathbf{b} \cdot \nabla)\mathbf{a} - (\mathbf{a} \cdot \nabla)\mathbf{b}
 \end{aligned}$$

If  $\mathbf{x}$  is the coordinate of a point with respect to some origin, with magnitude  $r = |\mathbf{x}|$ ,  $\mathbf{n} = \mathbf{x}/r$  is a unit radial vector, and  $f(r)$  is a well-behaved function of  $r$ , then

$$\begin{aligned}
 \nabla \cdot \mathbf{x} &= 3 & \nabla \times \mathbf{x} &= 0 \\
 \nabla \cdot [\mathbf{n}f(r)] &= \frac{2}{r}f + \frac{\partial f}{\partial r} & \nabla \times [\mathbf{n}f(r)] &= 0 \\
 (\mathbf{a} \cdot \nabla)\mathbf{n}f(r) &= \frac{f(r)}{r}[\mathbf{a} - \mathbf{n}(\mathbf{a} \cdot \mathbf{n})] + \mathbf{n}(\mathbf{a} \cdot \mathbf{n})\frac{\partial f}{\partial r} \\
 \nabla(\mathbf{x} \cdot \mathbf{a}) &= \mathbf{a} + \mathbf{x}(\nabla \cdot \mathbf{a}) + i(\mathbf{L} \times \mathbf{a})
 \end{aligned}$$

where  $\mathbf{L} = \frac{1}{i}(\mathbf{x} \times \nabla)$  is the angular-momentum operator.

In the following  $\phi$ ,  $\psi$ , and  $\mathbf{A}$  are well-behaved scalar or vector functions,  $V$  is a three-dimensional volume with volume element  $d^3x$ ,  $S$  is a closed two-dimensional surface bounding  $V$ , with area element  $da$  and unit outward normal  $\mathbf{n}$  at  $da$ .

$$\begin{aligned}
 \int_V \nabla \cdot \mathbf{A} d^3x &= \int_S \mathbf{A} \cdot \mathbf{n} da && \text{(Divergence theorem)} \\
 \int_V \nabla\psi d^3x &= \int_S \psi\mathbf{n} da \\
 \int_V \nabla \times \mathbf{A} d^3x &= \int_S \mathbf{n} \times \mathbf{A} da \\
 \int_V (\phi\nabla^2\psi + \nabla\phi \cdot \nabla\psi) d^3x &= \int_S \phi\mathbf{n} \cdot \nabla\psi da && \text{(Green's first identity)} \\
 \int_V (\phi\nabla^2\psi - \psi\nabla^2\phi) d^3x &= \int_S (\phi\nabla\psi - \psi\nabla\phi) \cdot \mathbf{n} da && \text{(Green's theorem)}
 \end{aligned}$$

In the following  $S$  is an open surface and  $C$  is the contour bounding it, with line element  $d\mathbf{l}$ . The normal  $\mathbf{n}$  to  $S$  is defined by the right-hand-screw rule in relation to the sense of the line integral around  $C$ .

$$\begin{aligned}
 \int_S (\nabla \times \mathbf{A}) \cdot \mathbf{n} da &= \oint_C \mathbf{A} \cdot d\mathbf{l} && \text{(Stokes's theorem)} \\
 \int_S \mathbf{n} \times \nabla\psi da &= \oint_C \psi d\mathbf{l}
 \end{aligned}$$

# Explicit Forms of Vector Operations

Let  $\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3$  be orthogonal unit vectors associated with the coordinate directions specified in the headings on the left, and  $A_1, A_2, A_3$  be the corresponding components of  $\mathbf{A}$ . Then

*Cartesian*  
( $x_1, x_2, x_3 = x, y, z$ )

$$\begin{aligned}\nabla\psi &= \mathbf{e}_1 \frac{\partial\psi}{\partial x_1} + \mathbf{e}_2 \frac{\partial\psi}{\partial x_2} + \mathbf{e}_3 \frac{\partial\psi}{\partial x_3} \\ \nabla \cdot \mathbf{A} &= \frac{\partial A_1}{\partial x_1} + \frac{\partial A_2}{\partial x_2} + \frac{\partial A_3}{\partial x_3} \\ \nabla \times \mathbf{A} &= \mathbf{e}_1 \left( \frac{\partial A_3}{\partial x_2} - \frac{\partial A_2}{\partial x_3} \right) + \mathbf{e}_2 \left( \frac{\partial A_1}{\partial x_3} - \frac{\partial A_3}{\partial x_1} \right) + \mathbf{e}_3 \left( \frac{\partial A_2}{\partial x_1} - \frac{\partial A_1}{\partial x_2} \right) \\ \nabla^2\psi &= \frac{\partial^2\psi}{\partial x_1^2} + \frac{\partial^2\psi}{\partial x_2^2} + \frac{\partial^2\psi}{\partial x_3^2}\end{aligned}$$


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*Cylindrical*  
( $\rho, \phi, z$ )

$$\begin{aligned}\nabla\psi &= \mathbf{e}_1 \frac{\partial\psi}{\partial\rho} + \mathbf{e}_2 \frac{1}{\rho} \frac{\partial\psi}{\partial\phi} + \mathbf{e}_3 \frac{\partial\psi}{\partial z} \\ \nabla \cdot \mathbf{A} &= \frac{1}{\rho} \frac{\partial}{\partial\rho} (\rho A_1) + \frac{1}{\rho} \frac{\partial A_2}{\partial\phi} + \frac{\partial A_3}{\partial z} \\ \nabla \times \mathbf{A} &= \mathbf{e}_1 \left( \frac{1}{\rho} \frac{\partial A_3}{\partial\phi} - \frac{\partial A_2}{\partial z} \right) + \mathbf{e}_2 \left( \frac{\partial A_1}{\partial z} - \frac{\partial A_3}{\partial\rho} \right) + \mathbf{e}_3 \frac{1}{\rho} \left( \frac{\partial}{\partial\rho} (\rho A_2) - \frac{\partial A_1}{\partial\phi} \right) \\ \nabla^2\psi &= \frac{1}{\rho} \frac{\partial}{\partial\rho} \left( \rho \frac{\partial\psi}{\partial\rho} \right) + \frac{1}{\rho^2} \frac{\partial^2\psi}{\partial\phi^2} + \frac{\partial^2\psi}{\partial z^2}\end{aligned}$$


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*Spherical*  
( $r, \theta, \phi$ )

$$\begin{aligned}\nabla\psi &= \mathbf{e}_1 \frac{\partial\psi}{\partial r} + \mathbf{e}_2 \frac{1}{r} \frac{\partial\psi}{\partial\theta} + \mathbf{e}_3 \frac{1}{r \sin\theta} \frac{\partial\psi}{\partial\phi} \\ \nabla \cdot \mathbf{A} &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_1) + \frac{1}{r \sin\theta} \frac{\partial}{\partial\theta} (\sin\theta A_2) + \frac{1}{r \sin\theta} \frac{\partial A_3}{\partial\phi} \\ \nabla \times \mathbf{A} &= \mathbf{e}_1 \frac{1}{r \sin\theta} \left[ \frac{\partial}{\partial\theta} (\sin\theta A_3) - \frac{\partial A_2}{\partial\phi} \right] \\ &\quad + \mathbf{e}_2 \left[ \frac{1}{r \sin\theta} \frac{\partial A_1}{\partial\phi} - \frac{1}{r} \frac{\partial}{\partial r} (r A_3) \right] + \mathbf{e}_3 \frac{1}{r} \left[ \frac{\partial}{\partial r} (r A_2) - \frac{\partial A_1}{\partial\theta} \right] \\ \nabla^2\psi &= \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial\psi}{\partial r} \right) + \frac{1}{r^2 \sin\theta} \frac{\partial}{\partial\theta} \left( \sin\theta \frac{\partial\psi}{\partial\theta} \right) + \frac{1}{r^2 \sin^2\theta} \frac{\partial^2\psi}{\partial\phi^2} \\ &\quad \left[ \text{Note that } \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial\psi}{\partial r} \right) \equiv \frac{1}{r} \frac{\partial^2}{\partial r^2} (r\psi). \right]\end{aligned}$$

$$\left. \begin{aligned} x'_0 &= \gamma(x_0 - \beta x_1) \\ x'_1 &= \gamma(x_1 - \beta x_0) \\ x'_2 &= x_2 \\ x'_3 &= x_3 \end{aligned} \right\} \quad (11.16)$$

where we have introduced the suggestive notation  $x_0 = ct$ ,  $x_1 = z$ ,  $x_2 = x$ ,  $x_3 = y$  and also the convenient symbols,

$$\left. \begin{aligned} \boldsymbol{\beta} &= \frac{\mathbf{v}}{c}, \quad \beta = |\boldsymbol{\beta}| \\ \gamma &= (1 - \beta^2)^{-1/2} \end{aligned} \right\} \quad (11.17)$$

The inverse Lorentz transformation is

$$\left. \begin{aligned} x_0 &= \gamma(x'_0 + \beta x'_1) \\ x_1 &= \gamma(x'_1 + \beta x'_0) \\ x_2 &= x'_2 \\ x_3 &= x'_3 \end{aligned} \right\} \quad (11.18)$$

$$\left. \begin{aligned} x'_0 &= \gamma(x_0 - \boldsymbol{\beta} \cdot \mathbf{x}) \\ \mathbf{x}' &= \mathbf{x} + \frac{(\gamma - 1)}{\beta^2} (\boldsymbol{\beta} \cdot \mathbf{x})\boldsymbol{\beta} - \gamma\boldsymbol{\beta}x_0 \end{aligned} \right\} \quad (11.19)$$

$$\left. \begin{aligned} A'_0 &= \gamma(A_0 - \boldsymbol{\beta} \cdot \mathbf{A}) \\ A'_\parallel &= \gamma(A_\parallel - \beta A_0) \\ A'_\perp &= A_\perp \end{aligned} \right\} \quad (11.22)$$

where the parallel and perpendicular signs indicate components relative to the velocity  $\mathbf{v} = c\boldsymbol{\beta}$ . The invariance from one inertial frame to another embodied through the second postulate in (11.15) has its counterpart for any 4-vector in the invariance,

$$A_0'^2 - |\mathbf{A}'|^2 = A_0^2 - |\mathbf{A}|^2 \quad (11.23)$$

For Lorentz transformations between  $S'$  and  $S$  reference frames, this refers to the  $S'$  frame that is moving with velocity  $\boldsymbol{\beta}$  relative to reference frame  $S$ .

Transforming  $\mathbf{E}$  and  $\mathbf{B}$  fields:

$$\mathbf{E}' = \gamma(\mathbf{E} + \boldsymbol{\beta} \times \mathbf{B}c) - \frac{\gamma^2}{\gamma+1} \boldsymbol{\beta}(\boldsymbol{\beta} \cdot \mathbf{E})$$

$$\mathbf{B}' = \gamma(\mathbf{B} - \boldsymbol{\beta} \times \mathbf{E}/c) - \frac{\gamma^2}{\gamma+1} \boldsymbol{\beta}(\boldsymbol{\beta} \cdot \mathbf{B})$$

you might use  $\frac{\gamma^2}{\gamma+1} = \frac{\gamma-1}{\beta^2}$  if you prefer.

The electromagnetic field tensor:

$$F^{\alpha\beta} = \begin{pmatrix} 0 & -E_x/c & -E_y/c & -E_z/c \\ E_x/c & 0 & -B_z & B_y \\ E_y/c & B_z & 0 & -B_x \\ E_z/c & -B_y & B_x & 0 \end{pmatrix}$$

Thus the gradient drift velocity is given by

$$\mathbf{v}_G = \frac{a^2}{2} \frac{1}{B_0} \left( \frac{\partial B}{\partial \xi} \right)_0 (\boldsymbol{\omega}_0 \times \mathbf{n})$$

An alternative form, independent of coordinates, is

$$\frac{\mathbf{v}_G}{\omega_B a} = \frac{a}{2B^2} (\mathbf{B} \times \nabla_{\perp} B)$$

$$\mathbf{v}_C \simeq c \frac{\gamma m}{e} v_{\parallel}^2 \frac{\mathbf{R} \times \mathbf{B}_0}{R^2 B_0^2} \quad (12.57)$$

With the definition of  $\omega_B = eB_0/\gamma mc$ , the curvature drift can be written

$$\mathbf{v}_C = \frac{v_{\parallel}^2}{\omega_B R} \left( \frac{\mathbf{R} \times \mathbf{B}_0}{RB_0} \right) \quad (12.58)$$

$$v_{\parallel}^2 = v_0^2 - v_{\perp 0}^2 \frac{B(z)}{B_0}$$