

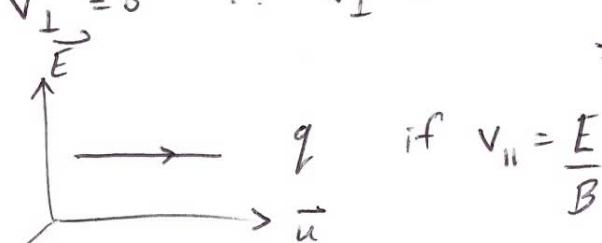
if  $|\frac{\vec{E}}{c}| < \vec{B}$ ,  $u = \frac{\vec{E}}{B}$  ← what does this case represent?

if  $|\frac{\vec{E}}{c}| > \vec{B}$ ,  $u = \frac{\vec{B}}{E}$  we can choose  $\vec{u} = \frac{\vec{E} \times \vec{B}}{B^2}$  to have  $S'$  frame with  $\vec{E}' = 0$ , only  $\vec{B}'$

but in  $S'$  if  $v_{||} = \frac{E}{B}$   $\therefore v'_{||} = 0$  then in  $S'$   $\vec{v}' = 0$

and  $u = \frac{\vec{E}}{B}$   $v_{\perp} = 0 \therefore v'_{\perp} = 0$  and only  $\vec{B}'$   
 $\Rightarrow$  no motion

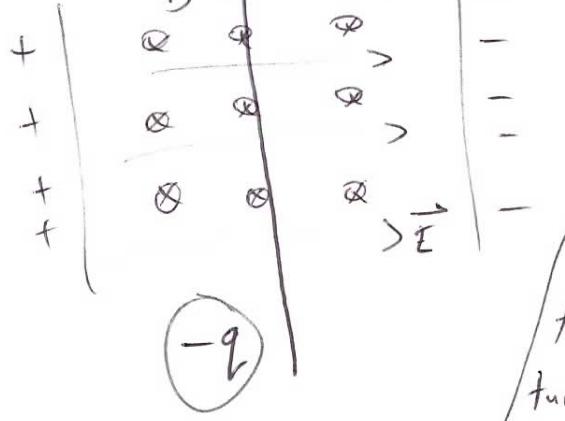
and in  $S$



This is the velocity selector (crossed  $\vec{E}$  and  $\vec{B}$  fields).

Combine with momentum selector ... leads to mass spec.

mass separation occurs



$$g^{\alpha\beta} F_{\alpha\beta} = -4 \vec{E} \cdot \vec{B}$$

if  $\vec{E} \cdot \vec{B} \neq 0$  then impossible to go to an inertial frame

with  $\vec{E}$  or  $\vec{B}$  zero  $\therefore$  if  $\vec{E} \cdot \vec{B} \neq 0$ ,  $\vec{E}$  and  $\vec{B}$  exist in simultaneously all Lorentz frames

Case 3: If  $\vec{E}$  has component parallel to  $\vec{B}$

then  $\vec{E} \cdot \vec{B} \neq 0$   
turns out  $\vec{E} \cdot \vec{B}$  is Lorentz scalar

we did uniform, static  $\vec{E}$  field only trivial  
 $\vec{B}$  " " 1st year physics  
 $\vec{E}, \vec{B}$  fields  $\perp$  considered ✓  
 $\vec{E}, \vec{B}$  with parallel components  $\rightarrow$  discussed

Non-uniform, static  $\vec{B}$  field

consider gentle variation (distance over which  $\vec{B}$  changes is large compared to the gyration radius  $a$ )

$\therefore$  spiralling along field lines with gyration radius set by local  $B$ -field strength

with next-order perturbation: orbit undergoes slow change described as drifting of guiding centre and slow variations of gyration (freq.)

case: gradient of spatial variation of  $\vec{B}$  is  $\perp$  to  $\vec{B}$

example  field around wire

$$\vec{B} = B(r) \hat{\phi}$$

gradient is in  $\hat{p}$  direction



motion parallel to  $\vec{B}$  remains uniform

1st order expansion

$$\vec{\omega}_B(\vec{x}) = \frac{q}{8\pi c} \vec{B}(\vec{x}) \approx \vec{\omega}_0 \left[ 1 + \frac{1}{B_0} \left( \frac{\partial B}{\partial \xi} \right)_0 \hat{n} \cdot \vec{x} \right]$$

( $\omega_B = \omega_0$  at the origin)

{ coordinate along  $\hat{n}$  - direction of gradient

$$\frac{d\vec{v}_\perp}{dt} = \vec{v}_\perp \times \vec{\omega}_B(\vec{x})$$

$$\vec{v}_\perp = \vec{v}_0 + \vec{v}_1$$

assume no motion along field lines

$$\frac{d\vec{v}_0}{dt} = \vec{v}_0 \times \vec{\omega}_0 \quad 0^{\text{th}} \text{ order}$$

$$\frac{d\vec{v}_1}{dt} \approx \left[ \vec{v}_1 + \vec{v}_0 (\hat{n} \cdot \vec{x}_0) \frac{1}{B_0} \left( \frac{\partial B}{\partial \xi} \right)_0 \right] \times \vec{\omega}_0 \quad \begin{matrix} \text{keep only} \\ 1^{\text{st}} \text{ order} \end{matrix}$$

$$\text{recall } \vec{V}_i = \omega_a (\hat{e}_1^i - i \hat{e}_2^i) e^{-i\omega_a t} + v_n \hat{e}_3^i$$

$$\vec{x}_o = v_{||} t \hat{e}_3 + i a (\hat{e}_1 - i \hat{e}_2) e^{-i\omega_a t}$$

$$\vec{\omega}_o \times \hat{e}_3 = 0$$

$$\vec{\omega}_o \times \hat{e}_2 = -\omega_o \hat{e}_1$$

$$\vec{\omega}_o \times \hat{e}_1 = \omega_o \hat{e}_2$$

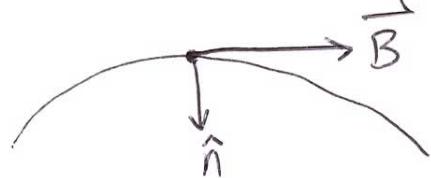
gives  $\vec{v}_i = -\vec{\omega}_o \times \vec{x}_o$

$$\frac{d\vec{v}_i}{dt} = \left[ \vec{v}_i - \frac{1}{B_0} \left( \frac{\partial B}{\partial \xi} \right)_o \vec{\omega}_o \times \vec{x}_o (\hat{n} \cdot \vec{x}_o) \right] \times \vec{\omega}_o$$

want to know about non-oscillating terms - net motion

averaged over cycles

$$\langle \vec{v}_i \rangle \equiv \vec{V}_G = \frac{1}{B_0} \left( \frac{\partial B}{\partial \xi} \right)_o \vec{\omega}_o \times \underbrace{\langle \vec{x}_o (\hat{n} \cdot \vec{x}_o) \rangle}_{\text{}}$$



orbits in plane containing  $\hat{n}$ ,  $\perp + \vec{B}$   
 $\hat{e}_1$ , out of page

$$\vec{x}_o = a (\sin \omega_B t \hat{e}_1 + \cos \omega_B t \hat{e}_2)$$

$$\langle \vec{x}_o (\hat{n} \cdot \vec{x}_o) \rangle = a^2 \langle \sin \omega_B t \hat{n} \cdot \cos \omega_B t \hat{e}_1 + \cos^2 \omega_B t \hat{n} \rangle$$

$$= \frac{a^2}{2} \hat{n}$$

gradient drift velocity

$$\vec{\omega}_B = \omega_B \vec{B}$$

$$\vec{\nabla}_B B = \hat{n} \frac{\partial B}{\partial \xi}$$

$$\vec{V}_G = \frac{a^2}{2} \frac{1}{B_0} \left( \frac{\partial B}{\partial \xi} \right)_o \vec{\omega}_o \times \hat{n}$$

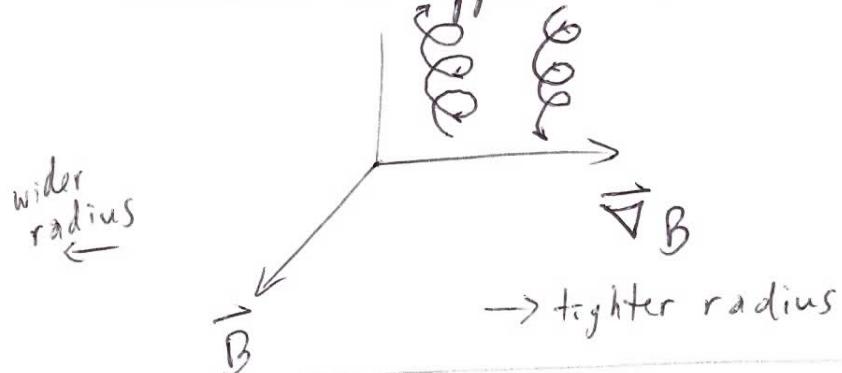
$$\frac{\vec{V}_G}{a \omega_B} = \frac{a}{2 B^2} \vec{B} \times \vec{\nabla}_B B$$

if  $a \left| \frac{\vec{\nabla} B}{B} \right| \ll 1$  distance over which  $\vec{B}$  changes is large compared to gyration radius  $a$

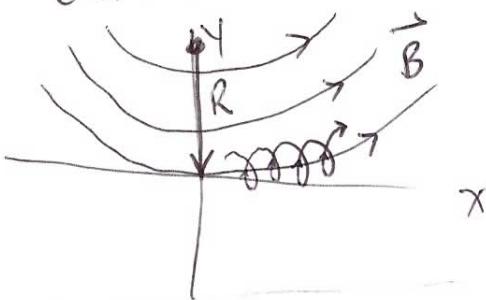
$v_g$  drift velocity is small compared to orbital velocity

$\therefore$  particle spirals rapidly around  $\vec{B}$  with  $\omega_B a$   
its center of rotation slowly moving perpendicular  
to both  $\vec{B}$  and  $\vec{\nabla} B$

$\rightarrow$  direction is opposite for  $(+)$  and  $(-)$  [it's in definition]  
for  $\omega_B = \frac{qB}{\gamma m}$



curvature of  $\vec{B}$  also causes drift radius of curvature



$$\vec{B} = B(\rho) \hat{\phi}$$

implies  $\vec{j} = 0$ , static

$$\vec{\nabla} \times \vec{B} = \frac{1}{\rho} \frac{\partial}{\partial \rho} \rho B_\phi = 0 \Rightarrow B_\phi \propto \frac{1}{\rho}$$

cylindrical coordinates

$\rho, \phi, z$

$$\left( \frac{e.g. I}{2\pi r} \right)$$

$$\vec{B} = B_0 \frac{R}{\rho} \hat{\phi} \quad \vec{\omega}_B = \omega_0 \frac{R}{\rho} \hat{\phi}$$

Lorentz force  $\vec{a} = \vec{\nabla} \times \vec{\omega}_B$   
acceleration

$$\omega_0 = \frac{qB_0}{\gamma m}$$

Force law  $\rightarrow$  equations of motion  $\rightarrow$  full solution

$V_{\parallel}$  motion in  $\hat{\phi}$  direction

$V_{\perp}$  in  $p, z$  plane

$$\vec{r} = p \hat{p} + z \hat{z}$$

$$\vec{v} = \dot{p} \hat{p} + p \dot{\phi} \hat{\phi} + \dot{z} \hat{z}$$

$$\vec{a} = \vec{v} \times \vec{\omega}_B = \frac{\omega_0 R}{p} \dot{p} \hat{z} - \frac{\omega_0 R}{p} \dot{z} \hat{p}$$

$$= (\ddot{p} - p \dot{\phi}^2) \hat{p} + (p \ddot{\phi} + 2\dot{p} \dot{\phi}) \hat{\phi} + \ddot{z} \hat{z}$$

$$(1) \quad \ddot{p} - p \dot{\phi}^2 = -\frac{\omega_0 R}{p} \dot{z}$$

$$(2) \quad p \ddot{\phi} + 2\dot{p} \dot{\phi} = 0 \Rightarrow p^2 \dot{\phi} = L = \text{constant} \quad \dot{L} = 0 \\ \equiv V_{\parallel} R \quad (\text{motion along field lines})$$

$$(3) \quad \ddot{z} = \frac{\omega_0 R}{p} \dot{p}$$

$$\text{integrate } \dot{z} = \omega_0 R \ln(p/R) + v_0$$

for helix with radius small compared to  $R$

$$p = R + x \rightarrow p/R = 1 + \frac{x}{R}$$

expand  $(p/R)^n$  and  $\ln(p/R)$  in powers of  $x/R$  (to 1st order)

$$\Rightarrow (1) \quad \ddot{x} - \frac{L^2}{R^3 (p/R)^3} = \ddot{x} - \frac{L^2}{R^3} \left[ 1 - 3\left(\frac{x}{R}\right) \right] = -\frac{\omega_0 R}{p} \left[ \omega_0 \left(\frac{x}{R}\right) + v_0 \right]$$

$$= -\omega_0 \left[ 1 - \left(\frac{x}{R}\right) \right] \left[ \omega_0 \left(\frac{x}{R}\right) + v_0 \right]$$

$$\ddot{x} - \frac{L^2}{R^3} \left[ 1 - 3\left(\frac{x}{R}\right) \right] = -\omega_0^2 x - \omega_0 v_0 \left[ 1 - \left(\frac{x}{R}\right) \right]$$

$$\boxed{\ddot{x} + \left(\omega_0^2 + 3\frac{v_0^2}{R^2}\right)x = \frac{v_{\parallel}^2}{R} - \omega_0 v_0}$$

SHM around a displaced equil<sup>m</sup>

$$\langle x \rangle = \frac{V_{\parallel i}^2}{\omega_0^2 R} - \frac{V_0}{\omega_0} \quad \text{where } V_{\parallel i} \ll \omega_0 R \\ \text{is assumed}$$

$$\langle \dot{z} \rangle = V_0 + \omega_0 R \left( \frac{x}{R} \right) \approx V_0 + \omega_0 x \approx \frac{V_{\parallel i}^2}{\omega_0 R}$$

curvature drift (average z-component velocity)

$V_c$  is  $\frac{V_{\parallel i}^2}{\omega_0 R}$  in the  $+\vec{z}$ -direction or  $\vec{R} \times \vec{B}$

so write  $\vec{V}_c = \underbrace{\frac{V_{\parallel i}^2}{\omega_0 R}}_{\text{same direction}} \frac{\vec{R} \times \vec{B}}{RB}$

~~as~~ as gradient drift  $V_{\perp} = \omega_B a$

$$\vec{V}_G = \frac{a^2 \omega_B}{2B^2} \vec{B} \times \vec{\nabla}_{\perp} B$$

for this example  $\vec{B} = B_0 \frac{R}{\rho} \hat{\phi}$ ;  $\vec{\nabla}_{\perp} B = -\frac{\vec{R}}{R^2} B$

$$\text{so } \vec{V}_G = \frac{a^2 \omega_B}{2B^2} \frac{\vec{R} \times \vec{B}(B)}{R^2} = \frac{\omega_B a^2}{2R} \left( \frac{\vec{R} \times \vec{B}}{RB} \right) \\ = \frac{V_{\perp}^2}{2\omega_B R} \left( \frac{\vec{R} \times \vec{B}}{RB} \right)$$

total drift velocity

$$\vec{V}_D = \vec{V}_c + \vec{V}_G = \frac{1}{\omega_B R} \left( V_{\parallel i}^2 + \frac{1}{2} V_{\perp}^2 \right) \left( \frac{\vec{R} \times \vec{B}}{RB} \right)$$

numbers (example) from plasma physics

$$v_{\parallel}^2 + \frac{1}{2} v_{\perp}^2 \approx \frac{kT}{m} ; \omega_B = \frac{eB}{8m}$$

Jackson gives:

$$v_0 [\text{cm/s}] = \frac{172 T [\text{K}]}{R [\text{m}] B [\text{gauss}]}$$

$R = 1$  meter

$$B = 10^3 \text{ gauss} \Rightarrow v_0 \approx 2 \times 10^3 \text{ cm/s}$$

$$T = 10^4 \text{ K} \quad (\text{1 eV energy}) \quad \approx 0(10) \text{ m/s}$$

$$v_{\parallel}, v_{\perp} \approx 100-1000 \text{ m/s} @ 10^4 \text{ K}$$

$\therefore$  drift velocity is 1-10% of thermal velocity  
(in this curved  $\vec{B}$  field geometry / example)